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(54) Title: CATIONIC POLYMERISATION OF 1-OLEFINS (57) Abstract A process for producing polyisobutene which has at least 70% of its unsaturation in the terminal position. The process uses a complex of boron trifluoride and alcohol as catalyst and a contact time of at least 8 minutes. The feature of the process is its ability to use longer contact times than used hitherto thereby facilitating its commercial operation and improving the control of such an operation. The high terminal unsaturation improves the reactivity of the polymer.		

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CATIONIC POLYMERISATION OF 1-OLEFINS

The present invention relates to a process for the cationic polymerisation of 1-olefins, and in particular to producing polyisobutenes which have a relatively high degree of terminal unsaturation.

5 Isobutene is a typical example of a 1-olefin. Methods of polymerising 1-olefins; e.g. isobutenes whether pure or in an isomeric mixture as in a C₄ raffinate, using a Friedel-Crafts type catalyst are well-known. Typical of such catalysts are the halides of aluminium, iron, zinc, titanium, tin, mercury and boron. These
10 catalysts have also been used in conjunction with small amounts of co-catalysts such as water, alcohol, sulphur dioxide, carboxylic acids, mineral acids, ethers and alkyl halides to enhance catalyst activity. The reaction has been carried out in the liquid or gaseous phases, batchwise or continuously, at temperatures ranging
15 from -100° to +100°C.

It is also known that the polymerisation of 1-olefins e.g. isobutene using a Friedel-Crafts type catalyst is a cationic process which proceeds through formation of intermediate carbonium ions.

The product of this reaction is generally a mixture of polymers
20 which have the unsaturated linkage in the terminal or internal position within the polymer. Conventional cationic processes generally yield a polymer with a relatively high proportion of internal unsaturation compared with polymers having terminal unsaturation. This is due to the "in situ" isomerisation of the
25 unsaturated linkage to an internal position and is inherent in most



cationic polymerisation processes. Internal unsaturation in olefin polymers is believed to be less desirable than terminal unsaturation because of the relatively lower chemical reactivity of internally unsaturated polymers when compared with terminally unsaturated polymers. This is especially true of the reactivity towards compounds such as maleic anhydride which forms an adduct with polyisobutene called polyisobutenyl succinic anhydride (PIBSA). These adducts are most valuable products and form the basis of the lubricating oil additives industry.

Of the cationic polymerisation catalysts used hitherto those containing boron trifluoride are known for their tendency to isomerise the unsaturation in the polymer product to an unreactive internal position. For instance, Puskas, I. et al in Journal of Polymer Science, Symposium No. 56, pp 191-202 (1976) have reviewed the relative effects of catalysts such as boron trifluoride and complexes thereof with cocatalysts such as acetic acid and water. In this article, the authors indicate that up to 40% vinylidene (i.e. terminal) unsaturation can be obtained with a contact time of 5-7 minutes. They conclude however that the longer the contact time the greater is the tendency for the vinylidene unsaturation in the polymer to be isomerised to an unreactive internal position.

This view also appears to be confirmed indirectly in an article by Mullin, M.A. et al in Khim i Tekhnol. Toplivo i Masel, vol 10, pp 23-26 (October 1965) in which a complex of boron trifluoride with methanol or a mixture of methanol and ethanol is disclosed as a catalyst for polymerising isobutene. This article discloses a very short contact time of 30-40 seconds which is indicative of the care necessary when using this catalyst.

The criticality of a short contact time in relation to the use of boron trifluoride catalyst for polymerising isobutene is also emphasised in GB 1592016 and EP-A-16312. The latter publication advocates vigorous control of contact time and catalyst concentration and stresses the need to have a contact time of below 40 seconds to avoid isomerisation of the double bonds.

It has now been found that a product predominating in terminal



unsaturation can be formed by using specific reaction conditions.

Accordingly, the present invention is a liquid phase process for the cationic polymerisation of a feedstock comprising 1-olefins in the presence of a boron trifluoride catalyst at a temperature
5 between -100 and +50°C characterised in that the catalyst is a preformed complex of boron trifluoride and an alcohol and the contact time of the polymerisation reaction is at least 8 minutes such that at least 70% of the unsaturated linkages in the polymer product are in the terminal position.

10 The term 'polymerisation' as used herein is intended to cover oligomerisation and the process is particularly suited to the production of oligomers such as dimers and trimers, and low molecular weight polymers of 1-olefins wherein the number average molecular weight (M_n) of the polymer may be from 100 to 15,000.

15 The hydrocarbon feedstock may be pure 1-olefin or a mixed feed containing the 1-olefin. 1-olefin feedstock containing 4 to 16 carbon atoms is preferred. If a pure olefin is used, which is gaseous under ambient conditions, it is necessary either to control the reaction pressure or to dissolve the olefin in a solvent medium
20 inert under the reaction conditions in order to maintain the olefin in the liquid phase. In the case of isobutene, which is typical of 1-olefins, the feedstock used in the polymerisation process may be pure isobutene or a mixed C₄ hydrocarbon feedstock such as that resulting from the thermal or catalytic cracking operation
25 conventionally known as a butadiene raffinate. This is a liquid when under pressure and hence no diluent is needed. The feedstock used may suitably contain between 10 and 100% by weight of isobutene. It is preferable to use a feedstock containing at least 15% by weight of isobutene and most preferably at least 40% by
30 weight of isobutene. The hydrocarbon feedstock used may contain in addition to isobutene between 10 and 20% by weight of butanes and/or between 20 and 40% by weight of normal butenes without adverse effect on the polyisobutene product.

The catalyst is a preformed complex of boron trifluoride and an
35 alcohol. The alcohol suitably contains 1-8 carbon atoms preferably



1-4 carbons atoms. Specific examples of such alcohols include methanol, ethanol, the propanols and the butanols. Of these, a complex between boron trifluoride and ethanol is most preferred.

5 In the complexes the molar ratio of boron trifluoride to the alcohol is suitably from 0.5:1 to 5:1, preferably from 0.5:1 to 2:1 and most preferably from 0.5:1 to 1:1.

Catalyst complexes with alcohols used in the present invention may be preformed by conventional techniques. For instance to produce a complex of boron trifluoride and ethanol, the boron
10 trifluoride is dissolved in an equimolar proportion of industrial ethanol. The complex so formed is then diluted with a solvent inert under the reaction conditions, e.g. dichloromethane. The solution of the complex so produced is used as the catalyst for the polymerisation reaction.

15 The polymerisation reaction is carried out in the liquid phase. The preformed catalyst complex is suitably introduced into the polymerisation reactor as a solution thereof in a solvent which is inert under the reaction conditions. The use of a solvent for the catalyst complex is only necessary to ensure a more effective
20 control of the concentration of the catalyst. However, it is possible to use the neat complex of boron trifluoride as such. Examples of suitable solvents include primary and secondary alkyl halides and aliphatic, alicyclic and cycloaliphatic hydrocarbons. Dichloromethane is a typical example of the solvent.

25 One of the surprising features of the present invention is that in spite of using boron trifluoride as a catalyst component, contact times above 1 minute can be used without risk of any substantial isomerisation of the double bonds in the product. By using a preformed complex of boron trifluoride, contact times in the range
30 8-70 minutes, preferably 12-20 minutes, can be used without adversely affecting the terminal unsaturation in the polymer. This is a significant feature because it enables more effective control of the reaction parameters and the concentration of the reactants used.

35 The polymerisation reaction is suitably carried out at a



temperature between -50 and +45°C, preferably between -15 and 40°C. The reaction may be carried out at a pressure in the range of 0.4 to 4 bar absolute. The process of the present invention is particularly suitable for producing polyisobutenes having a molecular weight of between 500 and 5000, even more preferably those having a molecular weight of between 750 and 2500. The significantly high proportion of terminal unsaturation in the polymers so produced are particularly suited for producing adducts with maleic anhydride which are eventually converted to the imides by reaction with appropriate amines for use as additives to lubricating oils.

The process of the present invention may be operated batchwise or continuously.

The present invention is further illustrated with reference to the following Examples.

Example 1

Feedstock Composition

	<u>Component</u>	<u>%</u>
20	Isobutane	3.0
	n-Butane	11.0
	Butene-1	27.9
	Isobutene	38.0
	cis-Butene-2	11.6
25	trans-Butene-2	8.5

Initiator

1:1 molar boron trifluoride : ethanol complex was prepared by dissolution of boron trifluoride in ethanol containing 0.1% water. This initiator was then used diluted in dichloromethane.

30 Polymerisation Conditions

Continuous feedstock addition rate : 1.1 Kg/hour
Continuous initiator addition rate : 0.019g mole/Kg feedstock
Reaction pressure : 650 mm Hg
Reaction residence time : 16 minutes
35 Reaction temperature : -5°C



Reaction poison

: Excess acetonitrile over
stoichiometric equivalence
of BF_3

Monomer Conversion % isobutene : 87

5 In a continuous process using the feedstock raffinate shown
above the catalyst complex solution was metered into the reactor
under the conditions shown above. After the contact time of
16 minutes the polymerisation reaction was terminated by using an
excess of 1% v/v acetonitrile in heptane which was continuously
10 added to the product collection vessels. The monomer conversion was
determined by on-line gas chromatography.

The catalyst complex was removed from the polymer/heptane
solution by an initial aqueous ammonia wash followed by two water
washes. The separated heptane solution was filtered and vacuum
15 distilled.

Polymer Yield

Polymer yield corresponded to 1 tonne per 54 g mole of
preformed boron trifluoride-ethanol complex. The total yield was
separated into two fractions by vacuum distillation at $200^\circ\text{C}/2\text{mm Hg}$
20 to give 95% yield of relatively high molecular weight fraction with
the remainder comprising predominantly dimer-hexamer oligomer
fraction.

Polymer Properties

The product, after removal of light polymer fraction, had a
25 viscosity of 1041 SSU at 98.9°C (BS188:1957) and a number average
molecular weight of 955 determined by vapour pressure osmometry.

^{13}C NMR analysis of the polymer enabled determination of
vinylidene end group structure as 76% of total. This compares
favourably with typical 1000 SSU viscosity polyisobutenes
30 commercially available and produced using AlCl_3 or Al alkyl chloride
based initiators which generally contain less than 10% vinylidene
unsaturation.

The process of Example 1 was repeated using different molar
ratios of the boron trifluoride ethanol complex. The reaction
35 conditions used and the results achieved are shown in Table 1 below.



The polymerisation process of Example 1 was repeated using (a) different molar ratios of the boron trifluoride ethanol complex but having a constant boron trifluoride concentration and (b) keeping the grade of the product polymer substantially constant. The reaction conditions used and the results achieved are shown in Table 1.

TABLE 1

Polymer Olefinic Endgroup Structure using Variable BF₃.EtOH Composition

15

BF ₃ .EtOH Composition		BF ₃ .EtOH used (as BF ₃) g mole/ tonne feedstock	% Isobutene Conv.	Polymer Grade ssu x 10 ⁻² at 98.89°C	% Olefinic Endgroup CH ₂ =CRR	
% BF ₃ by weight	Molar Ratio BF ₃ :EtOH					
(a) <u>At Constant BF₃ Conc.</u>						
25	59.5	1:1)	85	10	77
	52.5	0.75:1)	88	5	80
	49.6	0.67:1) ca 20	67	54	82
	47.3	0.61:1)	64	31	83
	46.3	0.59:1)	55	58	81
	42.2	0.5:1)	23	82	81
(b) <u>At Constant Polymer Grade</u>						
35	59.5	1:1	18.5	85	10	77
	55.3	0.91:1	20.0	89	9	76
	51.6	0.74:1	23.0	82	10	84
	51.6	0.74:1	25.0	85	9	80
	44.6	0.55:1	33.0	71	8	89
40						

Contact time : 15 - 20 minutes
Reaction temperature : -5°C

45



Example 3

A batch polymerisation was carried out as in Example 1 using the conditions shown in Table 2 below. The results are also shown in the Table.

TABLE 2

Batch Polymerisation using BDR Feedstock and BF₃.EtOH Initiator

Weight BDR g	Total BF ₃ .EtOH ml g mole/tonne feedstock	Total Polymer Yield g	% Light Polymer	Polymer Grade ssu x 10 ⁻² at 98.89°C	% Olefinic Endgroup CH ₂ =CRR
780	1.4 20.3	233.8	8.6	26	71

Conditions:

Temperature ca - 4°C

Reaction Time : 60 minutes



Example 4

Using the process of Example 1 the reproducibility of the method was tested and compared with a commercial aluminium chloride catalyst. The conditions used and the results achieved are shown in

5 Table 3 below.

TABLE 3

10 Reproducibility of Polymer Olefinic Endgroup Structure in ca 1000 ssu
Viscosity Grades Prepared by use of BF₃.EtOH

15		Z Olefinic Endgroup (¹³ C NMR Analyses)	
		CH ₂ = CRR	Me ₂ C = CHR
20	Results of)	74	12
	Individual)	77	12
	BF ₃ EtOH)	79	9
	Preparations	76	11
		77	11
25		78	11
	Average value	77	11
	Commercial	4	0
30	1000 SSUx10 ⁻²		
	Polymer		

Commercial 1000 SSUx10⁻²

Polymerisation Temp : ca + 25°C
 Initiator : AlCl₃ - HCl
 Residence Time : ca 30 mins

35 Conditions BF₃.EtOH

Polymerisation Temp : -5°C
 Residence Time : 15-20 mins
 Pressure : 635 mmHg

40

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Example 5

The process of Example 1 was repeated using a mixed isobutane/isobutene feedstock. The conditions used and the results achieved are shown in Table 4 below.

TABLE 4

Polymer Endgroup Structure using Isobutene/Isobutane Feedstock and
BF₃.EtOH Initiator

Polymerisation Conditions			Polymer Grade	
Temperature °C	BF ₃ .EtOH g/mole tonne feedstock	% Convn. Isobutene	ssu x 10 ⁻² at 98.89°C	% Olefinic Endgroup CH ₂ = CRR
-5	20	97	2	72
-8	12.5	88	5	76
-11	12.3	73	28	78

Feedstock : 37% Isobutene in Isobutane

Reactor Residence Time : 16 mins



Example 6

The process of Example 1 was repeated over varying contact times. The conditions used and results achieved are shown in Table 5 below.

TABLE 5

Effect of Reactor Residence Time upon Polymer Endgroup Structure -
Pilot Scale Polymerisation

Reactor Residence Time (mins)	% Olefinic Endgroup $\text{CH}_2 = \text{CRR}$
16	75
32	72
64	73

Catalyst : BF_3 .Ethanol
Temperature : -5°C
Pressure : 635 mmHg

The above results show that the process is capable of producing polymers with a terminal unsaturation of up to 90%, produces less light polymer, has a tighter molecular weight distribution and uses a more stable catalyst and can operate under milder conditions than used hitherto.



Claims:

1. A liquid phase process for the cationic polymerisation of a feedstock comprising 1-olefins in the presence of boron trifluoride as catalyst at a temperature between -100 and +50°C characterised in that the catalyst is a preformed complex of boron trifluoride and an alcohol and the contact time of the polymerisation reaction is at least 8 minutes such that at least 70% of the unsaturated linkages in the polymer product are in the terminal position.
2. A process according to claim 1 wherein the hydrocarbon feedstock comprising 1-olefins contains 4 to 16 carbon atoms in the 1-olefin.
3. A process according to claim 1 or 2 wherein the hydrocarbon feedstock is a butadiene raffinate.
4. A process according to any one of the preceding claims wherein the hydrocarbon feedstock contains at least 15% by weight of isobutene.
5. A process according to any one of the preceding claims wherein the process is carried out under pressure when the hydrocarbon feed is gaseous.
6. A process according to any one of the preceding claims 1 to 4 wherein the alcohol in the preformed complex catalyst contains from 1 to 8 carbon atoms.
7. A process according to claim 6 wherein the alcohol in the preformed complex catalyst contains 1 to 4 carbon atoms.
8. A process according to claim 7 wherein the alcohol in the preformed complex catalyst is ethanol.



9. A process according to any one of the preceding claims wherein the molar ratio of boron trifluoride to the alcohol is from 0.5:1 to 5:1.

10. A process according to any one of the preceding claims wherein
5 the contact time is between 8 and 70 minutes.

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INTERNATIONAL SEARCH REPORT

International Application No PCT/GB 84/00371

I. CLASSIFICATION OF SUBJECT MATTER (If several classification symbols apply, indicate all) ⁶ According to International Patent Classification (IPC) or to both National Classification and IPC IPC ⁴ : C 08 F 10/00; C 08 F 4/14											
II. FIELDS SEARCHED <div style="text-align: right; font-size: small;">Minimum Documentation Searched ⁷</div> <table style="width: 100%; border: none;"> <tr> <td style="width: 30%; border-bottom: 1px solid black; padding: 2px;">Classification System</td> <td style="border-bottom: 1px solid black; padding: 2px;">Classification Symbols</td> </tr> <tr> <td style="border: none; padding: 5px;">IPC⁴</td> <td style="border: none; padding: 5px;">C 08 F</td> </tr> </table> <div style="text-align: center; font-size: x-small; margin-top: 5px;">Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched ⁸</div>			Classification System	Classification Symbols	IPC ⁴	C 08 F					
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III. DOCUMENTS CONSIDERED TO BE RELEVANT ⁹ <table style="width: 100%; border: none;"> <tr> <th style="width: 10%; border-bottom: 1px solid black; font-size: x-small;">Category ⁹</th> <th style="width: 70%; border-bottom: 1px solid black; font-size: x-small;">Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²</th> <th style="width: 20%; border-bottom: 1px solid black; font-size: x-small;">Relevant to Claim No. ¹³</th> </tr> <tr> <td style="border: none; text-align: center; vertical-align: top; padding: 5px;">X</td> <td style="border: none; padding: 5px;">FR, A, 2222388 (MITSUI PETROCHEMICAL IND.) 18 October 1974 see claims 1,11,12; page 4, lines 10-15; page 5, lines 12-16; page 6, lines 5-9 --</td> <td style="border: none; text-align: center; vertical-align: top; padding: 5px;">1-10</td> </tr> <tr> <td style="border: none; text-align: center; vertical-align: top; padding: 5px;">X</td> <td style="border: none; padding: 5px;">DE, A, 704038 (I.G. FARBEN INDUSTRIE) 20 February 1941 see claim; page 1, lines 31-38 -----</td> <td style="border: none; text-align: center; vertical-align: top; padding: 5px;">6-8</td> </tr> </table>			Category ⁹	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²	Relevant to Claim No. ¹³	X	FR, A, 2222388 (MITSUI PETROCHEMICAL IND.) 18 October 1974 see claims 1,11,12; page 4, lines 10-15; page 5, lines 12-16; page 6, lines 5-9 --	1-10	X	DE, A, 704038 (I.G. FARBEN INDUSTRIE) 20 February 1941 see claim; page 1, lines 31-38 -----	6-8
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<div style="display: flex; justify-content: space-between; font-size: x-small;"> <div style="width: 45%;"> <p>• Special categories of cited documents: ¹⁴</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> </div> <div style="width: 45%;"> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"G" document member of the same patent family</p> </div> </div>											
IV. CERTIFICATION <table style="width: 100%; border: none;"> <tr> <td style="width: 50%; border-bottom: 1px solid black; padding: 2px;">Date of the Actual Completion of the International Search</td> <td style="width: 50%; border-bottom: 1px solid black; padding: 2px;">Date of Mailing of this International Search Report</td> </tr> <tr> <td style="border: none; text-align: center; padding: 5px;">8th February 1985</td> <td style="border: none; text-align: center; padding: 5px;">28 FEB. 1985</td> </tr> <tr> <td style="border-bottom: 1px solid black; padding: 2px;">International Searching Authority</td> <td style="border-bottom: 1px solid black; padding: 2px;">Signature of Authorized Officer</td> </tr> <tr> <td style="border: none; text-align: center; padding: 5px;">EUROPEAN PATENT OFFICE</td> <td style="border: none; text-align: center; padding: 5px;"> G.L.M. Kravdenberg </td> </tr> </table>			Date of the Actual Completion of the International Search	Date of Mailing of this International Search Report	8th February 1985	28 FEB. 1985	International Searching Authority	Signature of Authorized Officer	EUROPEAN PATENT OFFICE	 G.L.M. Kravdenberg	
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